

# **About Us**

UNIMOTION is a leading company in the industrial automation field, at a global level. Combining innovative engineering solutions – Unimotion helps companies of all sizes across a wide range of industrial segments. Unimotion develops Industry 4.0-enabled products and systems with leading quality, performance and value. Engineering, Production, Construction, Warehouse, Research & Development department; all this can be found under one roof. Thanks to years of experience and a consistent focus on automation technology, we are continually improving our products and implementing innovations that provide customers with many technical advantages. Our core values are precision, innovation, passion, and integrity. At Unimotion, our main goal is the satisfaction of every single customer with a commitment to deliver the impossible.

Unimotion sales team, technicians and experts are at your disposal to provide customized expertise and support. We look forward to meeting you and work on your special project.







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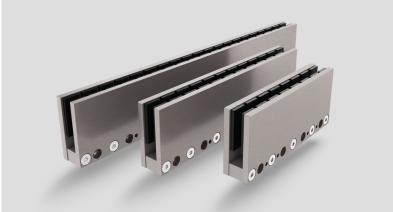
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**Product overview** 

# **PRODUCT OVERVIEW**

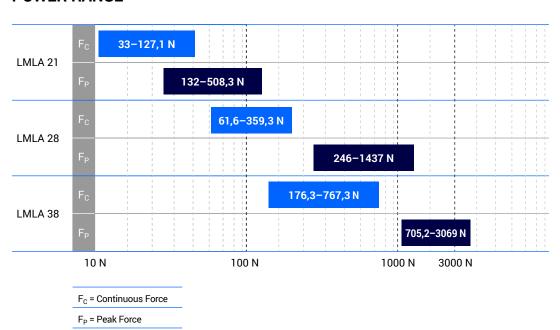
Welcome to the future of motion control with UNIMOTION cutting-edge Ironless linear motors. Designed to convert electrical energy directly into precise linear motion, these motors offer unrivaled speed, efficiency, and reliability across various industries and applications. Explore our catalog and revolutionize your projects with the seamless precision of UNIMOTION linear motor solutions.





Forcers Magnet plates

# **POWER RANGE**



# **Basic description**

Structural design			
Terms explanation			

Linear motors, like UNIMOTION Ironless Linear Motors, are an ideal substitute for pneumatic, hydraulic, belt, ball screw, or other types of drives. Linear motor drive systems do not require conversion from rotational to linear movement, because the movement is generated directly from the linear electromagnetic force. The linear motor driven systems, in comparison with the traditional linear units, are more compact, accurate, repeatable, faster, robust, reliable, generate less noise and, after all, require no maintenance. Linear motors are also known as "direct-drive" motors because the load is directly coupled onto them.

In contrast to iron core motors, UNIMOTION Ironless motors feature an ironless coil unit, eliminating attraction forces and cogging free between the motor and the magnet plate. This design offers numerous benefits, such as a lightweight framework, exceptional precision, dynamic responsiveness, high velocity, and swift acceleration and deceleration. These features collectively deliver unparalleled performance across diverse applications.

UNIMOTION linear motors are ideal for a variety of applications, ie.: actuators, robots, XYZ tables, positioning, assembly, tool machines, P&P machines, fiber optic machines, and many others. The main advantage of UNIMOTION linear motors is force density, which is 5-30 % higher compared to other competitors on the market. Thanks to our innovative design and state-of-the-art materials, we can offer our customers the industry-leading linear motor on the market for a competitive price.

Besides different motor sizes and versions, we offer magnet plates that cover all variants and types of all motor sizes.

Magnetic plates designed to accommodate various plate sizes, ensuring optimal length and stroke coverage.

Additionally, for each motor size, we are offering two speed variants:

- A low-speed variant, and
- A high-speed variant, which has a lower BEMF constant and is suitable for applications, requiring higher speed or lower supply voltage (110Vac).

Both solutions are air-cooled and with an extremely high force density, which offers a small and very compact design of the linear motion systems and units.

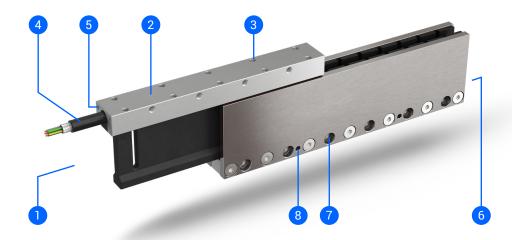
In order to allow an easy drive integration, we designed our own Hall sensor.

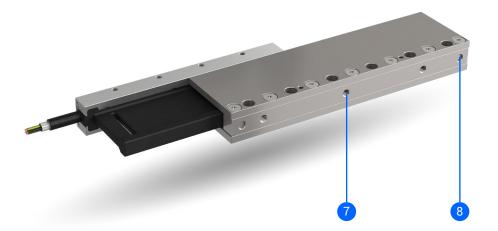
i For more information regarding the Hall sensor, please refer to page 26–28.

All UNIMOTION LMLA linear motors are CE and RoHS compliant.



# STRUCTURAL DESIGN





- 1 Forcer
- 2 Forcer body
- 3 Forcer mounting holes
- 4 Hybrid power and signal cable
- 5 Hall sensor mounting holes
- 6 Magnet plate
- 7 Magnet plate mounting holes
- 8 Magnet plate holes for centering ring or pin
- i For more information regarding the Hall sensor, please refer to page 26–28.

#### TERMS EXPLANATION

#### Supply voltage VDC:

A maximum allowed supply voltage, that can be applied to the motor windings.

#### Continuous force F<sub>C</sub>:

Force produced by the continuous current (IC) at next conditions:

- ambient temperature 20 °C
- attached to the mounting surface at 20 °C
- motor in continuous movement.

#### Peak force F<sub>P</sub>:

Force produced by the peak current (IP) for a duration of 1 second. The force is used for acceleration or deceleration.

#### Force constant K<sub>F</sub>:

Defines how much force is produced per unit of current. It is the ratio of the force to the motor phase current.

#### Motor constant K<sub>M</sub>:

The ratio of the motor force and square root of the power loss at 20 °C. The constant determines the motor's efficiency.

# Back EMF phase-phase constant K<sub>BEMF</sub>:

Defines the phase-to-phase voltage generated when the motor is moving at 1 m/s at the magnet temperature of 20 °C.

#### Continuous current Ic:

It corresponds to the continuous force (FC) and can be continuously applied to the motor at next conditions:

- ambient temperature 20 °C
- attached to the mounting surface at 20 °C
- motor in continuous movement.

#### Peak current la:

Corresponds to the peak force (FP) and can be applied to the motor for 1 second.

#### Resistance phase-phase R<sub>20</sub>:

Motor windings resistance measured phase to phase (line to line) at 20 °C.

#### Resistance phase-phase R<sub>125</sub>:

Motor windings resistance measured phase to phase (line to line) at 125 °C.

#### Induction phase-phase Lp:

Motor windings inductance measured phase-to-phase (line-to-line).

#### Electrical time constant t<sub>C</sub>:

The electrical time constant is the amount of time it takes for the current in the motor windings to reach 63 % of its rated value. The time constant is found by dividing inductance by resistance.

#### Max. winding temperature T<sub>max</sub>:

Defined as a maximum permissible temperature of the motor windings. During the normal operation, it is recommended that windings temperature does not exceed 80 % of  $T_{\text{max}}$ .

#### Thermal resistance R<sub>th</sub>:

Defines the heat transfer resistance from the motor windings to the environment at the defined plate (heatsink) and air dissipation.

#### Thermal resistance to heatsink R<sub>th-HS</sub>:

Defines the heat transfer resistance from the motor windings to the heatsink attached surface.

#### Magnet pitch τ:

Magnet pitch or pole pair length is the distance between two same polar magnets on the magnet plate.

#### Thermal time constant $\tau_{th}$ :

Defined as a time required for the winding to reach 63 % of the max. temperature at continuous current. This value is only applicable when the mounting surface is at the constant temperature.

How to order

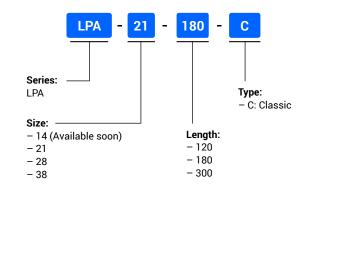
# **HOW TO ORDER**

#### Forcer order code

#### 04 Series: LMLA Type: - L: Low speed - H: High speed Size: Version: - 14 (Available soon) - 21 - 02 - 28 - 38 - 04 - 06 - 08 - 09 - 10 i Possible versions:

- LMLA 21: 02, 04, 06, 08 - LMLA 28: 02, 04, 06, 08, 12 - LMLA 38: 02, 04, 06, 09

#### Magnet plate order code



# Characteristics

LMLA 21	13
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# **LMLA 21**

# General technical data

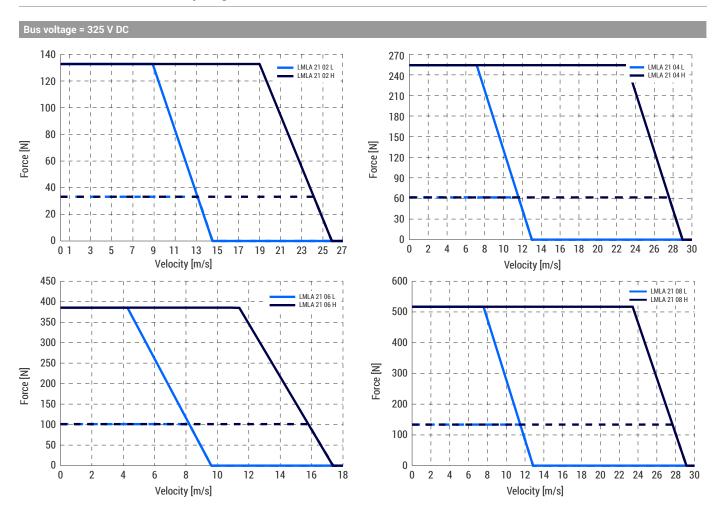
							LML	A 21			
				Versi	on 02	Versi	on 04	Versi	on 06	Versi	on 08
	PARAMETER	SYM	UNIT	Low speed	High speed	Low speed	High speed	Low speed	High speed	Low speed	High speed
	Max. supply voltage	$V_{DC}$	V (DC)				3.	40			
щ	Continuous force <sup>1</sup>	Fc	N	3	3	63	3,5	95	5,4	12	7,1
ANC ANC	Peak force (1 s) <sup>1</sup>	F <sub>P</sub>	N	1;	32	25	4,2	38	1,4	50	8,3
PERFORMANCE	Force constant	K <sub>F</sub>	$\frac{N}{A_{RMS}}$	24,5	13,8	27,5	12,2	36,7	20,6	27,5	12,2
PERF	Motor constant	K <sub>M</sub>	$\frac{N}{\sqrt{W}}$	4,9	4,9	6,8	6,9	8,4	8,4	9,7	9,7
	Back EMF phase- phase constant	K <sub>BEMF</sub>	VRMS (m/s)	14,1	7,9	15,9	7,1	21,2	11,9	15,9	7,1
	Continuous current	Ic	A <sub>RMS</sub>	1,4	2,4	2,3	5,2	2,6	4,6	4,6	10,4
	Peak current	I <sub>P</sub>	A <sub>RMS</sub>	5,4	9,6	9,2	20,8	10,5	18,5	18,5	41,6
)AL	Resistance at 20 °C phase-phase	R <sub>20</sub>	Ω	16,9	5,3	10,8	2,1	12,7	4,0	5,4	1,1
ECTRICAL	Resistance at 125 °C phase-phase	R <sub>125</sub>	Ω	23,8	7,5	15,3	3,0	17,9	5,7	7,6	1,5
H	Induction phase- phase	L <sub>P</sub>	mH	3,4	1,1	2,1	0,4	2,6	0,8	1,1	0,2
	Electrical time constant <sup>2</sup>	t <sub>C</sub>	ms	0,2	0,2	0,2	0,2	0,2	0,2	0,2	0,2
	Max. winding temperature	T <sub>max</sub>	°C				1:	25			
AL.	Max. allowed magnet plate temperature	T <sub>magnet</sub>	°C				7	0			
THERMAL	Thermal time constant	$ au_{th}$	s				6	5			
_	Thermal resistance	R <sub>th</sub>	K W	1,	61	0,	86	0,	58	0,	43
	Thermal resistance to heatsink	R <sub>th_HS</sub>	KW	1,1	20	0,5	96	0,3	397	0,2	298
	Forcer overall length	M <sub>L</sub>	mm	8	0	14	10	20	00	2	60
	Forcer overall width	M <sub>W</sub>	mm				2	.0			
	Forcer overall height	M <sub>H</sub>	mm				5	3			
_	Forcer mass	m <sub>m</sub>	kg	0,	22	0,	32	0,	42	0,	62
NICAL	Magnet plate weight	m <sub>S</sub>	kg m				4	,8			
MECHAN	Forcer wires cross-section	Sc	mm²			0	,5			0,	75
2	Sensor wires cross-section	S <sub>SC</sub>	mm²		0,14						
	Hybrid cable	L <sub>M</sub>	mm			· · · · · · · · · · · · · · · · · · ·	10	00		·	
	Magnet pitch	τ	mm				3	0			

 $<sup>^{\</sup>rm 1}$  Magnets at 20 °C.

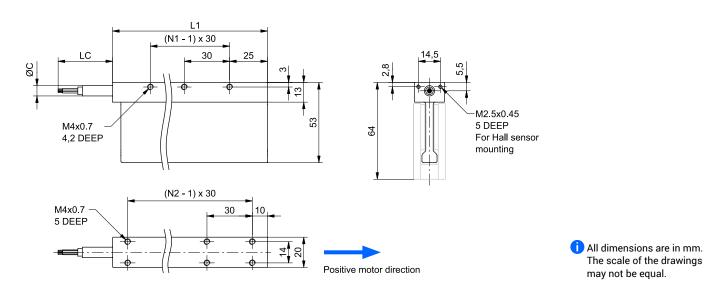
<sup>&</sup>lt;sup>2</sup> Windings at 20 °C.

 $<sup>\</sup>begin{tabular}{ll} \hline \textbf{1} The specifications were measured without forced cooling. For performance and electrical and thermal specifications tolerance is $\pm 10 \%$.} \\ \hline \end{tabular}$ 

# Force as a function of velocity diagrams



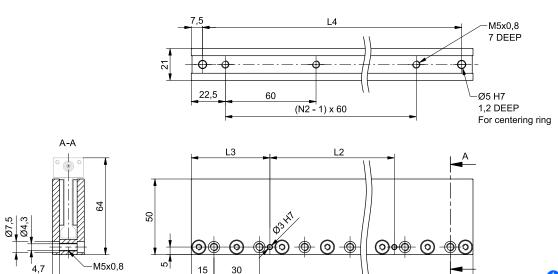
# **Forcer dimensions**



	LMLA		L1	LC	ØС	N1	N2	
Size	Version	Туре		[mm]		IN I	INZ	
	02	Н	80			2	3	
	J.	L						
	04	Н	140		7,1	4	5	
21	04	L	140	10001	.,.			
21	06	Н	200	1000		6	7	
	00	L	200			0	<u> </u>	
	08	Н	260		7,5	8	9	
	00	L	200		7,5	0	9	

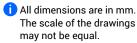
<sup>&</sup>lt;sup>1</sup> Standard cable length.

# **Magnet plate dimensions**



 $(N1 - 1) \times 30$ 

L1



Α

	LPA		L1	<b>L2</b> (±0,02)	L3	<b>L4</b> (±0,02)	N1	N2
Size	Length	Туре		[m	m]			
	120		120	60	37,5	105	4	2
21	180	С	180	76	52	165	6	3
	300		300	196	52	285	10	5

i 'N1' and 'N2' are the number of mounting holes along the motor direction.

i 'N1' and 'N2' are the number of mounting holes along the motor direction.

# **LMLA 28**

# General technical data

								LML	A 28				
				Versi	on 02	Versi	on 04	Versi	on 06	Versi	on 08	Versi	on 12
	PARAMETER	SYM	UNIT	Low speed	High speed								
	Max. supply voltage	V <sub>DC</sub>	V (DC)				1	34	40				
щ	Continuous force <sup>1</sup>	F <sub>C</sub>	N	61	,6	11	9,7	17	9,6	23	9,5	35	9,3
NC	Peak force (1 s) <sup>1</sup>	F <sub>P</sub>	N	24	46	4	79	7	18	9!	58	14	37
PERFORMANCE	Force constant	K <sub>F</sub>	$\frac{N}{A_{RMS}}$	35,2	15,7	35,2	15,7	52,8	23,5	62,6	31,3	70,4	31,3
PERF	Motor constant	K <sub>M</sub>	$\frac{N}{\sqrt{W}}$	7,7	7,7	10,9	10,9	13,4	13,4	15,4	15,4	18,9	18,9
	Back EMF phase- phase constant	K <sub>BEMF</sub>	VRMS (m/s)	20,3	9,0	20,3	9,0	30,5	13,6	36,2	18,1	40,7	18,1
	Continuous current	Ic	A <sub>RMS</sub>	1,8	3,9	3,4	7,7	3,4	7,7	3,8	7,7	5,1	11,5
	Peak current	Ι <sub>P</sub>	A <sub>RMS</sub>	7,0	15,7	13,6	30,6	13,6	30,6	15,3	30,6	20,4	45,9
SAL	Resistance at 20 °C phase-phase	R <sub>20</sub>	Ω	13,9	2,7	6,9	1,4	10,4	2,1	11,0	2,7	9,3	1,8
ECTRICAL	Resistance at 125 °C phase-phase	R <sub>125</sub>	Ω	19,6	3,9	9,8	1,9	14,7	2,9	15,5	3,9	13,1	2,6
品	Induction phase- phase	L <sub>P</sub>	mH	4,3	0,9	2,2	0,4	3,2	0,6	3,4	0,9	2,9	0,6
	Electrical time constant <sup>3</sup>	t <sub>C</sub>	ms	0,3	0,3	0,3	0,3	0,3	0,3	0,3	0,3	0,3	0,3
	Max. winding temperature	T <sub>max</sub>	°C			'	·	1:	25		'		
IAL	Max. allowed magnet plate temperature	T <sub>magnet</sub>	°C					7	0				
THERMAL	Thermal time constant	$ au_{th}$	s					7	7				
_	Thermal resistance	R <sub>th</sub>	K W	1,1	10	0,5	590	0,3	190	0,2	290	0,2	200
	Thermal resistance to heatsink	R <sub>th_HS</sub>	K W	0,7	'88	0,4	117	0,2	278	0,2	208	0,1	38
	Forcer overall length	M <sub>L</sub>	mm	8	0	14	40	20	00	20	50	38	30
	Forcer overall width	M <sub>W</sub>	mm					2	7				
	Forcer overall height	M <sub>H</sub>	mm					81	,8				
بِ	Forcer mass	m <sub>m</sub>	kg	0	,3	0	,6	0,	74	0,	96	1,3	39
NICA	Magnet plate weight	m <sub>S</sub>	kg m					9	,9				
MECHANICAL	Forcer wires cross- section	S <sub>C</sub>	mm²		0	,5				0,	75		
2	Sensor wires cross- section	S <sub>SC</sub>	mm²					0,	14				
	Hybride cable	L <sub>M</sub>	mm	1000									
	Magnet Pitch	τ	mm					3	0				

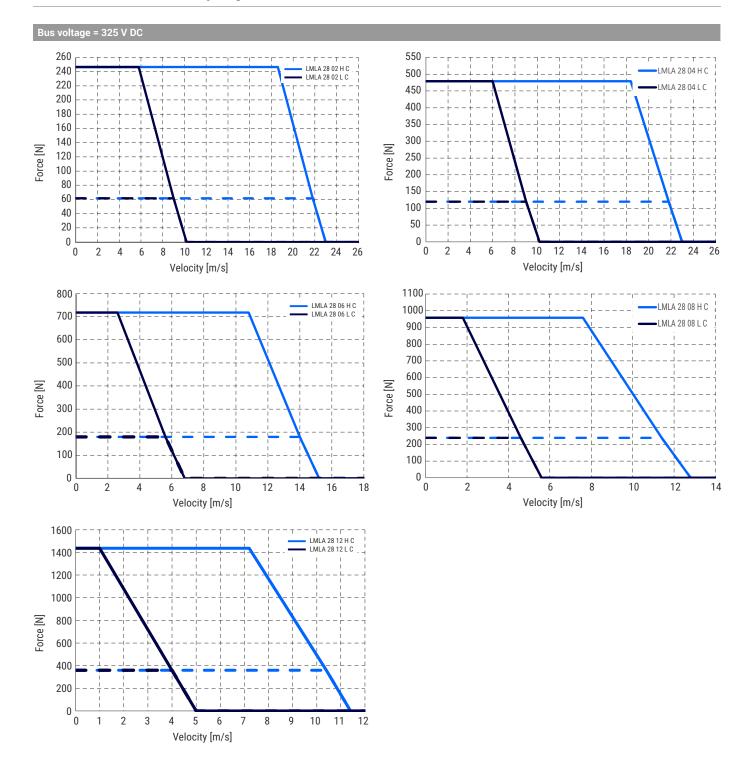
<sup>&</sup>lt;sup>1</sup> Magnets at 20 °C. <sup>2</sup> RMS at 0 A

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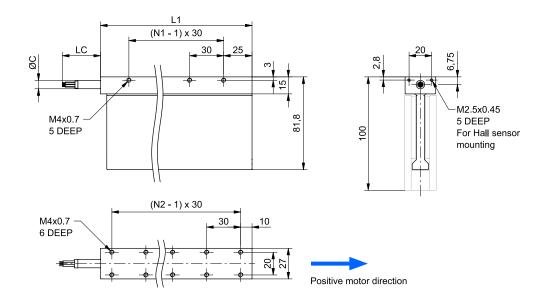
1 The specifications were measured without forced cooling. For performance and electrical and thermal specifications tolerance is  $\pm\,10$  %.

 $<sup>^{\</sup>rm 3}$  Windings at 20 °C.

# Force as a function of velocity diagrams



# **Forcer dimensions**



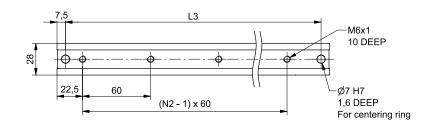
i All dimensions are in mm. The scale of the drawings may not be equal.

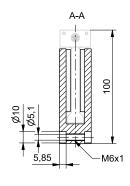
	LMLA		L1	LC	ØC	NI	N2	
Size	Version	Туре		[mm]		N1	142	
	02	Н	80			2	3	
	02	L	00		7,1			
	04	Н	140		7,1	4	5	
	04	L	140					
28	06	Н	200	1000¹		6	7	
20		L	200	1000				
	08	Н	260		7,5	8	9	
	00	L	200		1,5	0		
	12	Н	380			12	13	
	12	L	300			12	13	

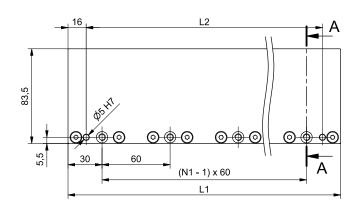
i 'N1' and 'N2' are the number of mounting holes along the motor direction.

<sup>&</sup>lt;sup>1</sup> Standard cable length.

# **Magnet plate dimensions**







	LPA		L1	<b>L2</b> (±0,02)	<b>L3</b> (±0,02)	N1	N2
Size	Length	Туре		[mm]			
	120		120	88	105	2	2
28	180	С	180	148	165	3	3
	300		300	268	285	5	5

i 'N1' and 'N2' are the number of mounting holes along the motor direction.

# **LMLA 38**

# General technical data

							LML	A 38			
				Versi	on 02	Versi	on 04	Versi	on 06	Versi	on 09
	PARAMETER	SYM	UNIT	Low speed	High speed						
	Max. supply voltage	V <sub>DC</sub>	V (DC)				340				
щ	Continuous force <sup>1</sup>	F <sub>C</sub>	N	17	6,3	34	41	511,5		767,3	
NO	Peak force (1 s) <sup>1</sup>	F <sub>P</sub>	N	70	5,2	13	64	20	46	30	69
PERFORMANCE	Force constant	K <sub>F</sub>	N A <sub>RMS</sub>	68,2	30,7	68,2	30,7	92,0	46,0	102,3	46,0
PERF	Motor constant	K <sub>M</sub>	N/W	16,0	16,0	22,7	22,7	27,8	27,8	34,0	34,0
	Back EMF phase- phase constant	K <sub>BEMF</sub>	$\frac{V_{RMS}}{(m/s)}$	39,4	17,7	39,4	17,7	53,1	26,6	59,1	26,6
	Continuous current	Ic	A <sub>RMS</sub>	2,6	5,8	5,0	11,1	5,6	11,1	7,5	16,7
	Peak current	I <sub>P</sub>	A <sub>RMS</sub>	10,3	23,0	20,0	44,5	22,2	44,5	30,0	66,7
CAL	Resistance at 20 °C phase-phase	R <sub>20</sub>	Ω	12,0	2,4	6,0	1,2	7,3	1,8	6,0	1,2
ELECTRICAL	Resistance at 125 °C phase-phase	R <sub>125</sub>	Ω	17,0	3,4	8,5	1,7	10,3	2,6	8,5	11,7
□	Induction phase- phase	L <sub>P</sub>	mH	10,9	2,2	5,5	1,1	6,6	1,7	5,5	1,1
	Electrical time constant <sup>3</sup>	t <sub>C</sub>	ms	0,9	0,9	0,9	0,9	0,9	0,9	0,9	0,9
	Max. winding temperature	T <sub>max</sub>	°C				12	25			
AL	Max. allowed magnet plate temperature	T <sub>magnet</sub>	°C				7	0			
THERMAL	Thermal time constant	$ au_{th}$	s				11	17			
_	Thermal resistance	R <sub>th</sub>	K W	0,5	590	0,3	310	0,2	10	0,1	40
	Thermal resistance to heatsink	R <sub>th_HS</sub>	K W	0,4	115	0,2	223	0,1	49	0,0	199
	Forcer overall length	M <sub>L</sub>	mm	1:	50	2	70	39	90	5	70
	Forcer overall width	M <sub>W</sub>	mm				3	7			
	Forcer overall height	M <sub>H</sub>	mm				10	4,9			
ب	Forcer mass	m <sub>m</sub>	kg		1	1	,8	2	,6	3	,7
NICA	Magnet plate weight	m <sub>S</sub>	<u>kg</u> m				14	l,2			
MECHANICAL	Forcer wires cross- section	Sc	mm²		0	,5			0,	75	
2	Sensor wires cross- section	S <sub>SC</sub>	mm²	2 0,14							
	Hybride cable	L <sub>M</sub>	mm				10	00			
	Magnet Pitch	τ	mm				6	0			

<sup>&</sup>lt;sup>1</sup> Magnets at 20 °C.

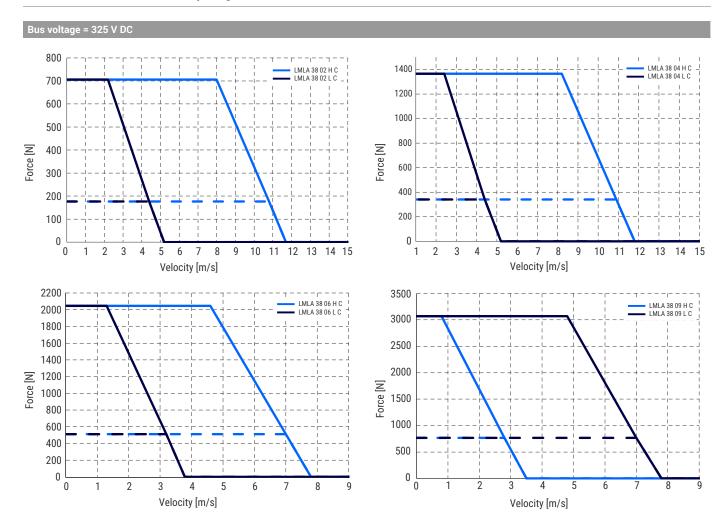
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<sup>&</sup>lt;sup>2</sup> RMS at 0 A.

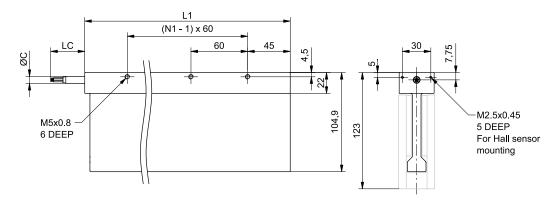
 $<sup>^{\</sup>rm 3}$  Windings at 20 °C.

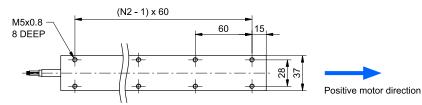
 $<sup>\</sup>ensuremath{\mbox{\bf i}}$  The specifications were measured without forced cooling. Electrical specifications tolerance is  $\pm$  10 %.

# Force as a function of velocity diagrams



# **Forcer dimensions**





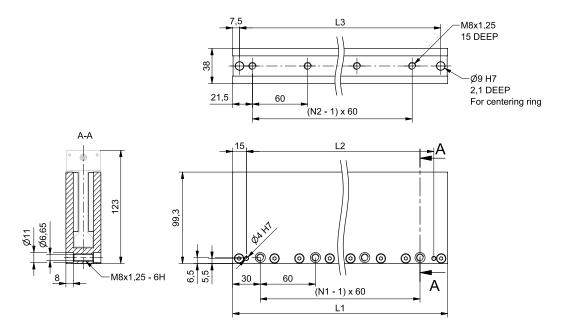
i All dimensions are in mm. The scale of the drawings may not be equal.

	LMLA		L1	LC	ØС	N1	N2	
Size	Version	Туре		[mm]		IN I	N2	
	02	Н	150			2	3	
	02	L	130		7,1		3	
	04	Н	270		7,1	4	5	
38	04	L	270	1000¹		4	3	
30	06	Н	390	1000	7,5	6	7	
		L	390			0	, 	
	09	Н	570		1,5	9	10	
	09	L	370			9	10	

i 'N1' and 'N2' are the number of mounting holes along the motor direction.

<sup>&</sup>lt;sup>1</sup> Standard cable length.

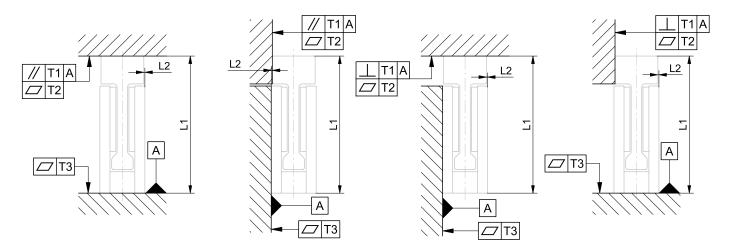
# **Magnet plate dimensions**



	LPA L1 L2 (±0,02				<b>L3</b> (±0,02)	N1	N2
Size	Length	Туре		[mm]			
	120		120	90	105	2	2
38	180	С	180	150	165	3	3
	300		300	270	285	5	5

i 'N1' and 'N2' are the number of mounting holes along the motor direction.

# **MOUNTING TOLERANCES**



i We recommend using a thermally conductive paste between the forcer and heatsink to ensure a better heat transfer.

LMLA	<b>L1</b> (±0,1)	L2	T1	T2	Т3
21	64	0,5 ± 0,05	0,05	0,05	0,05/500 mm
28	100	0,5 ± 0,10	0,10	0,10	0,05/500 mm
38	123	0,5 ± 0,10	0,10	0,10	0,05/500 mm

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# **ELECTRICAL DATA**

#### Temperature sensor

LMLA linear motors are equipped with a temperature sensor which is generally used for overheating protection. The sensor type is STS1 1000 3 which is thermally coupled with the U winding.

The STS1 1000 3 sensor is commonly used for monitoring motor temperature and can be use for limitation of maximum operational temperature.

For continuous operation, it is recommended that the motor temperature does not exceed 80 % of the maximum allowed motor temperature (125 °C).

#### STS1 1000 3 Thermistor

The linear motor is equiped with a STS1 1000 3 thermistor. This sensor features a positive temperature coefficient, and its characteristic curve exhibits near-linearity across the entire operating range. With a thermal time constant of approximately 6 seconds.

The temperature of the windings can be calculated from the current resistance of the STS1 1000 3 sensor with the use of the following equation.

$$T = 100 + \frac{\sqrt{\alpha^2 - 4 \cdot \beta + 4 \cdot \beta \cdot \frac{R_T}{R_{25}}} - \alpha}{2 \cdot \beta}$$

R <sub>T</sub>	Current sensor reading	[Ω]
α	6,7 · 10 <sup>-3</sup>	[K-1]
β	1,5 · 10-5	[K-1]
R <sub>25</sub>	1000	[Ω]

In the table below, resistance values of STS1 1000 3 at specific temperatures are presented.

T [°C]	20	30	40	50	60	70	80	90	100	110	120	125	130
R [Ω]	561	603	647	695	747	804	866	931	1000	1071	1142	1177	1213

Resistance of STS1 at ambient temperature (25 °C)	582 Ω
Normal operating STS1s resistance (25 °C-120 °C)	< 1142 Ω
Cut-off resistance of STS1	> 1177 Ω

#### Wiring specifications

In the following table wiring specifications of the forcer is presented.

Parameter	Symbol	Wire colour	
Motor phase U	U	brown	
Motor phase V	V	black	
Motor phase W	W	gray	
Grounding	GND	yellow/green	
Temperature sensor	T <sub>temp+</sub>	yellow	
Temperature sensor	T <sub>temp</sub> –	green	
Cable shield	Earth	Shield	

# **LMLA Hall sensor**

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#### **Description**

UNIMOTION offers a Hall sensor which was specifically developed for the LMCA linear motors. The sensor utilizes existing magnet feedback which allows an unmatched accuracy to price ratio. Its main advantage is integration of the analog¹ and digital sensors into one housing.



Our Hall sensor can be used for a cost-effective solution when the position accuracy demands are not very high. Repeatable accuracy is in the range of  $+/-30 \,\mu m$  whilst absolute accuracy is in the range of  $+/-250 \,\mu m$ . With the integration of both sensors, analog<sup>1</sup> is used for exact position control, where digital is used for commutation. A combination of both offers the customer a free "wake & shake" operation feature.

The sensor is equipped with 10 highly flexible shielded wires, which are suitable for use in the energy chains. The digital sensor generates the U, V, and W signal outputs with a 120° phase shift while the analog¹ sensor generates sine and cosine signals with an amplitude of 1 VPP. For the best resistance against the EMC, the signals are differential, ie.: sine: A+, A- and cosine: B+, B-.

Our Hall sensor enables easy and precise mounting which results in an ideal alignment of the sensors and motor windings.

### **Specifications**

#### Absolute maximum ratings:

Parameter	Unit	Min	Max
Power supply voltage V <sub>CC</sub>	V <sub>DC</sub>	-0,3	6
Output pin current U, V, W, A+, A-, B+, B-	mA	0	100
Operating junction temperature, T <sub>J</sub>	°C	-15	60
Storage temperature, T <sub>stg</sub>	°C	-25	85

#### Recommended operating conditions:

Parameter	Unit	Min	Max
Power supply voltage V <sub>CC</sub>	$V_{DC}$	4,9	5,5
Power supply current	mA	30	50
Output current	mA	_	20
Output voltage A+ to A- and B+ to B-	$V_{pp}$	0,8	1,2
Operating junction temperature, T <sub>J</sub>	°C	-15	60
Storage temperature, T <sub>stg</sub>	°C	-25	85

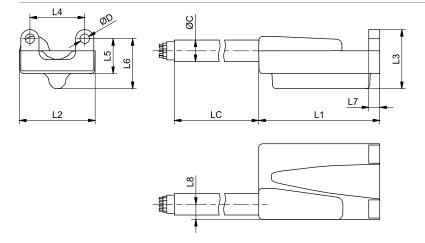
#### Technical specifications:

Parameter	Unit	Value
Sensor accuracy <sup>1</sup>	μm	±250
Repeatability	μm	±30
Hysteresis	μm	±10
Signal period	mm	30
Cable (high flex)	/	10 x 0,14 mm <sup>2</sup>
Cable bending radius (fixed installation)	mm	26,8
Cable bending radius (flexible installation)	mm	50,25

<sup>&</sup>lt;sup>1</sup> In case of drive compensation, the accuracy can be improved.

<sup>&</sup>lt;sup>1</sup> Version with analog signals: Available soon

# **Dimensions**



i All dimensions are in mm.
The scale of the drawings may not be equal.

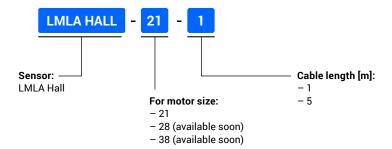
LMLA HALL	L1	L2	L3	L4	L5	L6	L7	L8	ØD	LC	ØС
Size		[mm]									
21 <sup>2</sup>	32	20	15,6	14,5	9,2	13,2	2,9	4	2,5	1000¹	5,7

 $<sup>^{\</sup>mathrm{1}}$  Standard cable length. For different lengths, please refer to the "Hall sensor – How to order" section.

# Wiring specifications

Parameter	Symbol	Wire colour
Analog hall output A+	A+	Yellow
Analog hall output A-	A-	Green
Analog hall output B+	B+	Violet
Analog hall output B-	B-	White
Digital hall output U	U	Gray
Digital hall output V	V	Black
Digital hall output W	W	Pink
Power supply +5 V <sub>DC</sub>	+5 V <sub>DC</sub>	Red
Power supply GND	GND	Blue
NC	Service	Brown
Cable shield	Earth	Shield

#### How to order



<sup>&</sup>lt;sup>2</sup> Sizes 14, 28 and 38 will be available soon.

# Motor selection example

I. Definition of the motion profile	30
II. Calculation of continuous and peak forces	32
III. Motor selection	33
Selection example	34

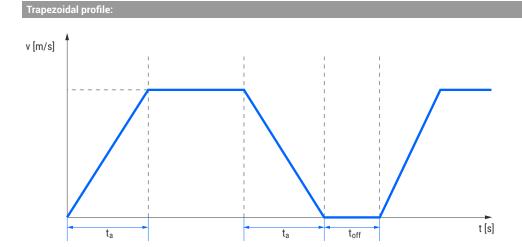
#### Motor selection guide:

The proper motor selection is done in three steps:

- I. Definition of the motion profile
- II. Calculation of continuous and peak forces
- III. Motor selection

# I. Definition of the motion profile

There is a wide range of different motion profiles which can be expressed by basic kinematic equations. The most commonly used motion profiles are trapezoidal and triangular.



# Moving input data:

L	Moving distance (stroke)	[m]
t	Moving time	[s]
t <sub>a</sub>	Acceleration time	[s]
t <sub>off</sub>	Pause	[s]

Average velocity:

$$v = \frac{L}{\cdot}$$

Maximum velocity:

$$v_{max} = \frac{L}{t - t_a}$$

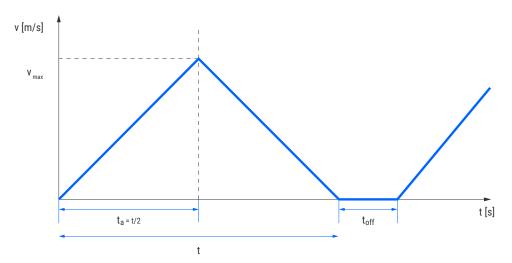
Acceleration/deceleration:

$$a = \frac{v_{max}}{t_{o}}$$

Variables used in equations:

v	Average velocity	[m/s]
V <sub>max</sub>	Maximum velocity	[m/s]
L	Moving distance	[m]
t	Moving time	[s]
ta	Acceleration time	[s]
а	Acceleration/deceleration	[m/s <sup>2</sup> ]

# Triangular profile:



# Moving input data:

L	Moving distance (stroke)	[m]
t	Moving time	[s]
ta	Acceleration time	[s]
t <sub>off</sub>	Pause	[s]

Average velocity:

$$v = \frac{L}{t}$$

Maximum velocity:

$$v_{max} = \frac{a}{t_a}$$

Acceleration/deceleration:

$$a = \frac{4 \cdot L}{t^2}$$

Variables used in equations:

v	Average velocity	[m/s]
V <sub>max</sub>	Maximum velocity	[m/s]
L	Moving distance	[m]
t	Moving time	[s]
t <sub>a</sub>	Acceleration time	[s]
а	Acceleration/deceleration	[m/s <sup>2</sup> ]

# II. Calculation of continuous and peak forces

When velocity and acceleration are defined, we can proceed to the calculation of continuous and peak forces which the motor has to overcome.

#### Input parameters:

m <sub>load</sub>	Mass of load	[kg]
k <sub>f</sub>	Friction coefficient	
α	Inclination angle	[°]

#### Peak force can be calculated by using the following equation:

 $F_p = F_{mass} + F_{fri} + F_{incl}$ 

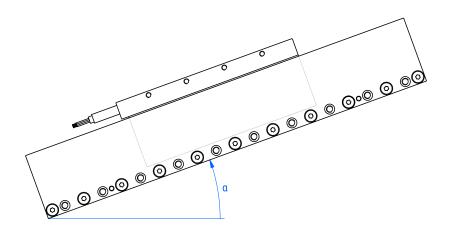
 $F_{mass} = a \cdot m_{load}$ 

 $F_{fri} = k_f(g \cdot m_{load} \cdot cos\alpha)$ 

 $F_{incl} = m_{load} \cdot g \cdot \sin \alpha$ 

#### Variables used in equations:

F <sub>P</sub>	Peak force	[N]
а	Acceleration	[m/s <sup>2</sup> ]
m <sub>load</sub>	Mass of load	[kg]
k <sub>f</sub>	Friction coefficient	
g	Gravitational constant (9,81)	[m/s <sup>2</sup> ]
α	Inclination angle	[°]
F <sub>incl</sub>	Inclination force (if the motor is placed horizontally ( $\alpha = 0^{\circ}$ ) the F <sub>incl</sub> is 0)	[N]



# Continuous force can be calculated by following equation:

$$F_{C} = \sqrt{\frac{F_{p}^{2} \cdot t_{a} + (F_{fri} + F_{incl})^{2} \cdot (t - 2t_{a}) + (F_{mass} + F_{incl} - F_{fri})^{2} \cdot t_{a}}}{t + t_{off}}$$

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#### III. Motor selection

#### Defining the motors RMS and MAX current:

$$I_{MAX} = \frac{F_P}{K_F}$$

$$I_{RMS} = \frac{F_C}{V}$$

< I<sub>P</sub> from the motor specification.

$K_F$	•	·
$I_{RMS} = \frac{F_C}{K_F}$	$<$ I $_{\rm C}$ from the	motor specification.

i We recommend a safety factor where Ip and  $I_C$  are 30 % higher than  $I_{MAX}$  and  $I_{RMS}$ .

#### Variables used in equations:

F <sub>P</sub>	Peak force	[N]
F <sub>C</sub>	Continuous force	[N]
K <sub>F</sub>	Force constant (you can find it in the motor specifications)	[N/A <sub>RMS</sub> ]

#### Motor voltage calculation:

For the proper motor selection, the correct voltage must be calculated with the below equation:

$$V_{mot} = \sqrt{\left(\sqrt{2} \; \frac{v_{max} \cdot K_{BEMF}}{\sqrt{3}} + \frac{F_P}{K_F} \cdot R_{20} \cdot \frac{\sqrt{2}}{2}\right)^2 + \left(\sqrt{2} \cdot 2\pi \cdot \frac{F_P \cdot L_P}{K_F \cdot 2 \cdot \tau}\right)^2}$$

#### Variables used in equations:

V <sub>max</sub>	Maximum velocity	[m/s]
K <sub>BEMF</sub>	Motor induction voltage phase-phase RMS (listed in the motor specifications)	[V/m/s]
K <sub>F</sub>	Force constant (listed in the motor specifications)	[N/A <sub>RMS</sub> ]
F <sub>P</sub>	Peak force	[N]
R <sub>20</sub>	Phase-phase resistance (listed in the motor specifications)	[Ω]
L <sub>P</sub>	Phase-phase inductance	[H]
τ	Magnet pitch (listed in the motor specifications)	[m]

Available drive voltage can be calculated with the following equations:

$$V_{\text{drive\_SVM}} = \frac{\sqrt{2} V_{\text{supply}} [\text{VAC}]}{\sqrt{3}}$$
; In the case of AC power supply

 $V_{drive\_SVM} \frac{V_{supply}[VDC]}{\sqrt{3}}$ ; In the case of DC power supply

#### Variables used in equations:

V <sub>supply</sub>	Drive supply voltage (for example 230 V AC or 325 V DC)	[V <sub>RMS</sub> ]
V <sub>drive_SVM</sub>	The available voltage that can be applied to the linear motor	[V]

#### Motor selection condition:

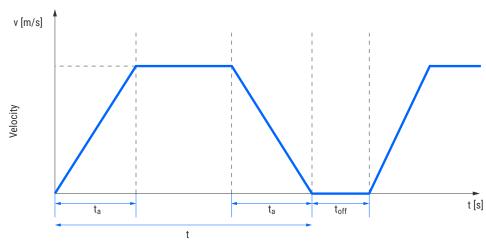
Drive voltage must be higher than the maximum voltage of the motor.

 $V_{mot} < V_{drive\_SVM}$ 

A safety factor where V<sub>drive\_SVM</sub> is 30 % higher than V<sub>mot</sub> is recommended.

# Selection example

#### I. Definition of the motion profile



- Moving distance L = 2 m
  Moving time t = 1 s
  Acceleration time t<sub>a</sub> = 0,25 s
- Pause t<sub>off</sub> = 0,5 s
- Mass of load  $m_{load}$  = 5 kg Friction coefficient  $k_f$  = 0,01
- $-\alpha = 0^{\circ}$

Average velocity:

$$v = \frac{L}{t} = \frac{2}{1} = 2 \text{ m/s}$$

Maximum velocity:

$$v_{max} = \frac{L}{t - t_a} = \frac{2}{1 - 0.25} =$$
**2,67 m/s**

Acceleration/deceleration:

$$a = \frac{v_{max}}{t_a} = \frac{2,67}{0,25} = 10,67 \text{ m/s}^2$$

# II. Continuous and peak force calculation

#### Peak force:

$$F_{mass} = a \cdot m_{load} = 10,67 \cdot 5 =$$
**53,3 N**

$$F_f = k_f(g \cdot m_{load} \cdot cos\alpha) = 0.01 \cdot (9.81 \cdot 5 \cdot cos0) = 0.5 \text{ N}$$

$$F_{incl}$$
 =  $m_{load} \cdot g \cdot sin\alpha$  = **0 N**

$$F_p = F_{mass} + F_f + F_{incl} = 53,3 + 0,5 + 0 = 53,8 \text{ N}$$

#### **Continuous force:**

$$F_C = \sqrt{\frac{F_p^2 \cdot t_a + (F_{fri} + F_{inc})^2 \cdot (t - 2t_a) + (F_{mass} + F_{incl} - F_{fri})^2 \cdot t_a}{t + t_{off}}}$$

$$= \sqrt{\frac{53,89^2 + 0,25 + (0,5 + 0)^2 \cdot (1 - 2 \cdot 0,25) + (53,3 + 0 - 0,5)^2 \cdot 0,25}{1 + 0,5}} = 30,8 \text{ N}$$

#### III. Motor selection

Maximum motor current:

$$I_{MAX} = \frac{F_P}{K_F} = \frac{53.8}{27.51} = 1,96 \text{ A}_{RMS} < 9.2 \text{ A}_{RMS}$$

**Continuous motor current:** 

$$I_{RMS} = \frac{F_C}{K_F} = \frac{30.8}{27.51} = 1,12 \text{ A}_{RMS} < 2.3 \text{ A}_{RMS}$$

Motor related parameters can be found in the motor specifications (example see LMLA21\_4L):

- K<sub>F</sub> = 27,5 N/A<sub>RMS</sub>
   I<sub>C</sub> = 2,3 A<sub>RMS</sub>
   I<sub>P</sub> = 9,2 A<sub>RMS</sub>

#### Motor voltage calculation:

For a proper motor selection, voltage is also important, which must be applied by the servo drive. Maximum voltage is calculated by:

$$\begin{split} V_{mot} &= \sqrt{\left(\sqrt{2} \, \frac{v_{max} \cdot K_{BEMF}}{\sqrt{3}} + \frac{F_P}{K_F} \cdot R_{20} \cdot \frac{\sqrt{2}}{2}\right)^2 + \left(\sqrt{2} \cdot 2\pi \cdot \frac{F_P \cdot L_P}{K_F \cdot 2 \cdot \tau}\right)^2} \\ &= \sqrt{\left(\sqrt{2} \, \frac{2.67 \cdot 15.9}{\sqrt{3}} + \frac{53.8}{27.51} \cdot 10.8 \cdot \frac{\sqrt{2}}{2}\right)^2 + \left(\sqrt{2} \cdot 2\pi \cdot \frac{53.8 \cdot 0.00215}{27.51 \cdot 2 \cdot 30}\right)^2} = \textbf{49.6 V} \end{split}$$

Motor related parameters can be found in the motor specification:

- $K_F = 27.5 \text{ N/A}_{RMS}$
- $K_{BEMF} = 15.9 \text{ V/m/s}$   $R_{20} = 10.8 \Omega$
- $L_{\rm P} = 2.1 \, \text{mH}$
- $\tau = 30 \text{ mm}$

#### Available drive voltage:

$$V_{\text{supply}} = 230 V_{AC}$$

$$V_{drive\_SVM} = \frac{\sqrt{2} \ V_{supply}}{\sqrt{3}} = \frac{\sqrt{2} \ \cdot 230}{\sqrt{3}} = 187.8 \ V > 49.6 \ V$$